Basic Linear System Dynamics

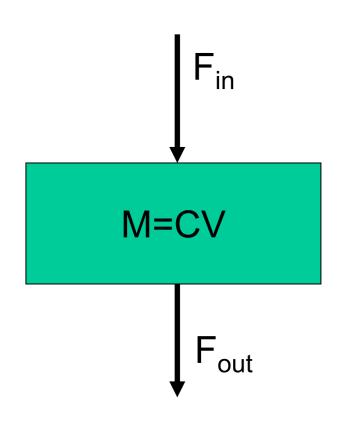
Reservoirs & Fluxes
Steady-states & Transients
Residence & Response times
System Gain & Frequency Response
Feedbacks, Loops & Oscillations

Originally by John Shepherd, Modified by Kevin Oliver, 2010

Basic System Dynamics

- ♦ Most theory is for *linear* systems
 - *Non-linear* systems are much trickier, but approximations to linear systems can be obtained for *small perturbations*.
- ◆ Concepts: Fluxes and inventories
- ◆ *Steady-state* (equilibrium) & *transient* (disequilibrium) conditions (*statics vs. dynamics*)
- ◆ Reservoir effects: finite response times
 - Residence times, Transit times, Mixing times, Reaction times, etc
- ◆ Multiple/continuous reservoirs (e.g. the ocean)
 - Distributions of response times & ages

Single reservoir residence time & response time (1)



V = volume of reservoir (fixed)

C = concentration (quantity per unit volume)

M = total mass or quantity (= inventory) (= "standing stock")

F=flux (quantity per unit time)

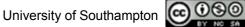
NB: may (often) be per unit area

Change = Input - Output

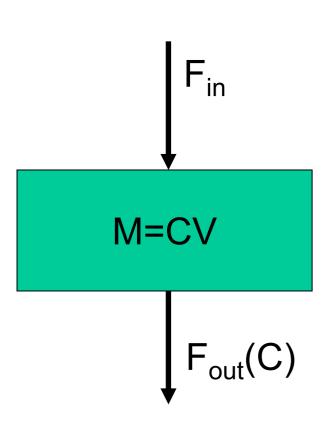
$$\therefore dM/dt = F_{in} - F_{out}$$
at *steady-state* dM/dt = 0

$$\therefore$$
 $F_{in} = F_{out}$ and $\tau_{res} = M/F_{in} = M/F_{out}$

NB: Quantity may be measured as mass, moles, etc, etc... One *must* ensure dimensional consistency (i.e. the *units* check out OK)



Single reservoir residence time & response time (2)



In general F_{in} and F_{out} may depend on C e.g. in a first-order removal rate process

$$F_{out} = k'C = kCV$$
 where $k' = kV$, where $[k] = 1/[time]$
$$dM/dt = d(CV)/dt = F_{in} - kCV$$

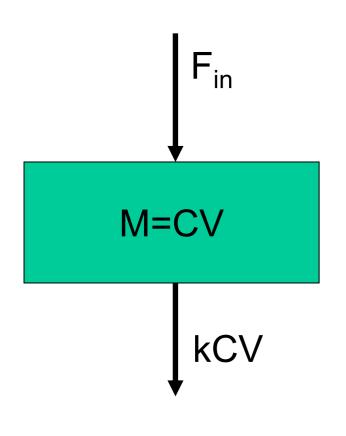
$$dC/dt = S - kC$$
 where $source\ term\ S = (F_{in}/V)$ (quantity per unit volume per unit time)

Solution is *exponential approach to steady-state* $C = (S/k) \{1 - \exp(-kt)\}$ Response time = residence time = $\tau_{res} = 1/k$

NB: (1) for radio-active decay $k = \lambda$ (the radio-active decay constant)

(2) for multiple (*parallel*) removal processes $k_{tot} = k_1 + k_2 + k_3 \dots$ and hence $\tau_{res} = 1 / \{1/\tau_1 + 1/\tau_2 + 1/\tau_3\}$ like "resistances in parallel" in this case the *fastest* process (with the smallest τ value) dominates

Single reservoir residence time & response time (3)

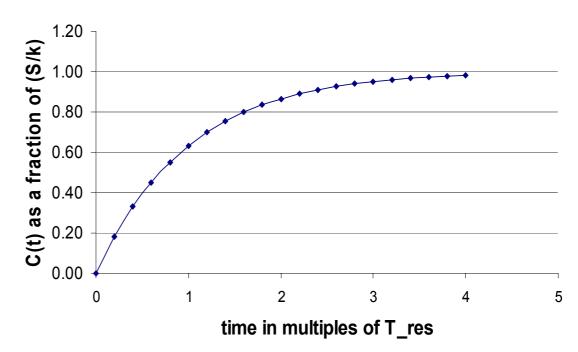


Solution is exponential approach to steady-state

$$C = (S/k) \{1 - \exp(-kt)\}$$

Response time = residence time = $\tau_{res} = 1/k$

Response of a single reservoir



Characteristic system timescales

- Residence time; $T_{res} = 1/k (= 1/ \lambda)$
- ♦ Transit time (advection); $T_{adv} = L/u$
 - Where L = length scale, u = velocity
- Mixing time (diffusion); $T_{mix} = L^2/2K$
 - Where K = diffusion coefficient
 - Usually due to turbulence
 - May differ (a lot) in different spatial dimensions
 - Horizontal mixing is a lot faster than vertical mixing
 - K values are $\sim 10^8$ times larger in horizontal than in vertical
- Scavenging/deposition time; $\tau_{dep} = D/v_{dep}$
 - Where D = depth scale, $v_{dep} = deposition velocity$
 - Also applies to gas exchange; so $T_g = D/v_g$
- **♦** NB: Flux (per unit area) = velocity × concentration
 - (with concentration expressed as quantity *per unit volume*)
- ♦ With processes <u>in series</u>, the <u>slowest</u> process dominates

Multiple reservoirs "Mass" fluxes and exchanges

- ♦ Consider simple exchanges between reservoirs
- Exchange time $\tau_{exch} = Vol/Q$
 - Where $Q = u_{exch} \times Area$
 - Dimensions of Q are [Volume/Time]
 - i.e "mass" or volume flux, e.g. m³/sec or Sv
 - Q and u_{exch} may be due to advective or diffusive exchange (or both)
- ◆ For multiple reservoirs (e.g. in a box model)
 - For the i^{th} box, with volume V_i , and exchange coefficients Q_{ij} between the i^{th} and the j^{th} boxes

$$au_i = V_i / \sum_j Q_{ij}$$

So the exchanges operate in parallel, and the fastest dominates

Basic System Dynamics

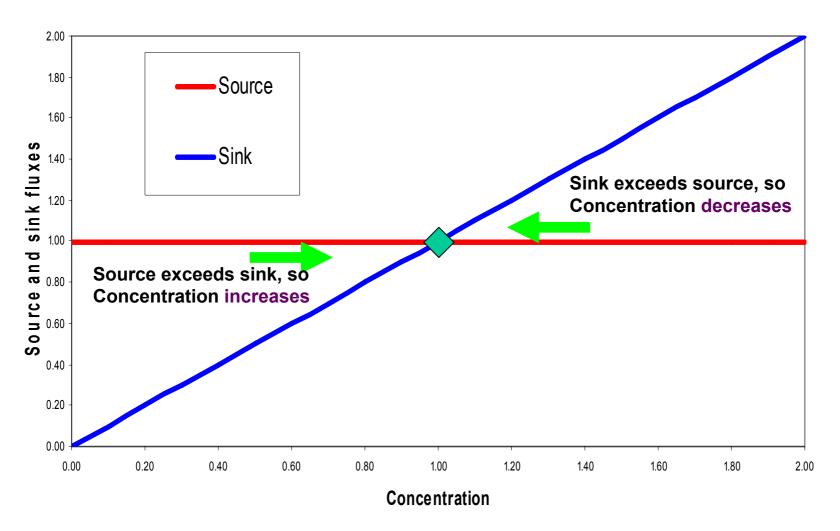
Feedbacks, Loops & Oscillations

Linear System Dynamics: Feedbacks

- ◆ *Positive* feedbacks if these outweigh negative feedbacks:
 - multiple alternative states (separated by **repellors**)
 - hysteresis & rapid transitions (switching)
- ♦ Negative feedbacks if these outweigh positive feedbacks:
 - if *instantaneous*: stabilisation, stable states (attractors)
 - if *delayed*: may get resonance (amplification) & possibly oscillations (at characteristic frequencies)

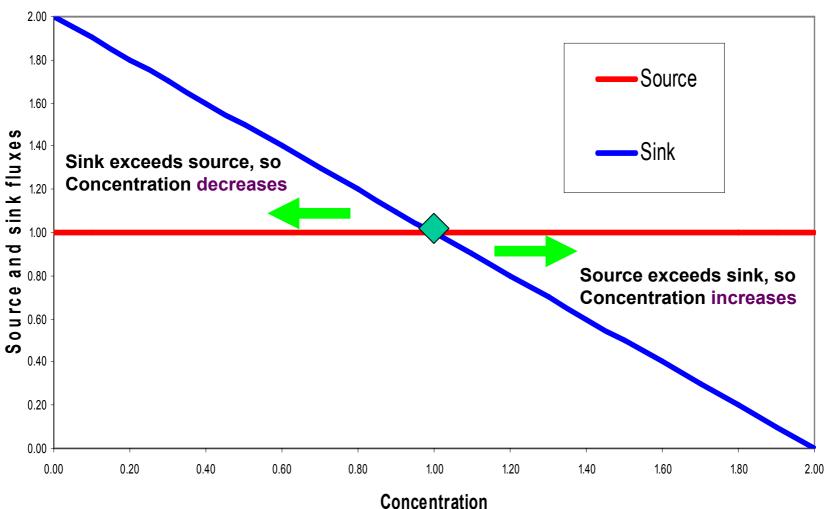
Negative feedback: constant source, but sink flux *increases* with concentration

Balance of source and sink

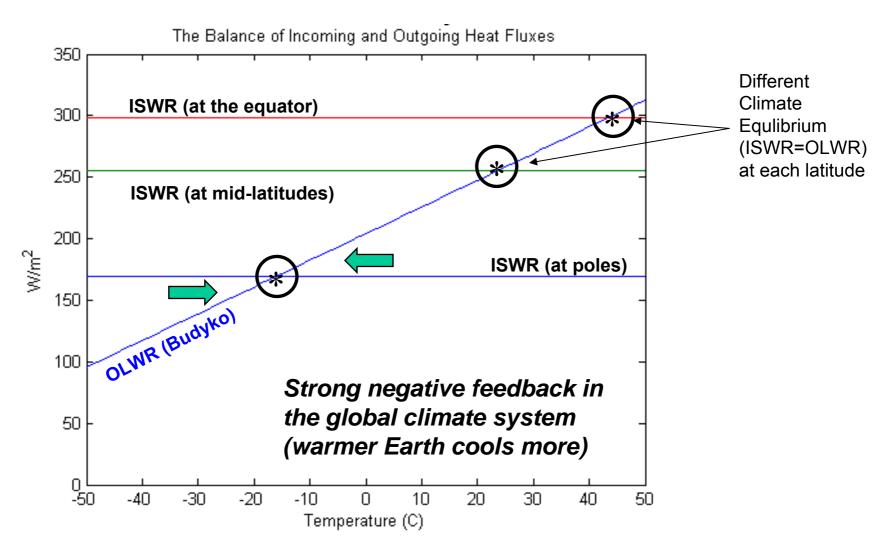


Positive feedback: constant source, but sink flux *decreases* with concentration

Balance of source and sink



Equating ISWR and OLWR (see Lecture 7)

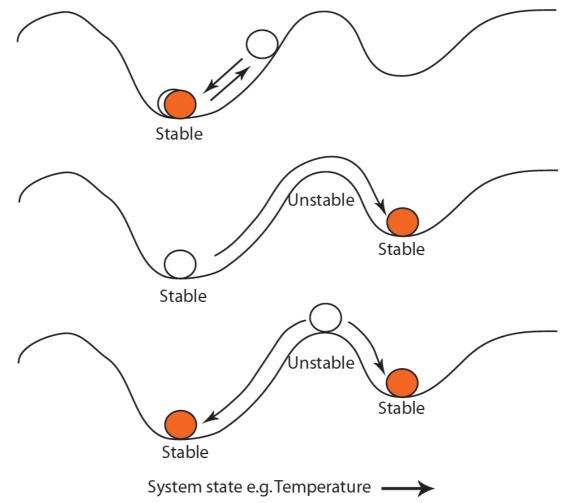


- If $T < T^*$, ISWR > OLWR => warmer
- If $T > T^*$, ISWR < OLWR => cooler

Feedbacks & response to perturbations

- ◆ If the concentration is perturbed from equilibrium...
- ♦ With *negative* feedback, the sink term changes so as to reduce the perturbation
 - And so restore the equilibrium
 - : the feedback is *stabilising*
 - The system "seeks" a stable steady-state
- ♦ With *positive* feedback, the sink term changes so as to increase the perturbation
 - And so increase the dis-equilibrium
 - : the feedback is *destabilising*
 - If positive feedbacks outweigh negative feedbacks, the system perturbation grows irreversibly (though in practice the linearity of the system usually breaks down instead)

Stable, and unstable equilibria (strictly, *stationary points*) of the system



Negative Feedback

A = Open loop gain

f = feedback fraction

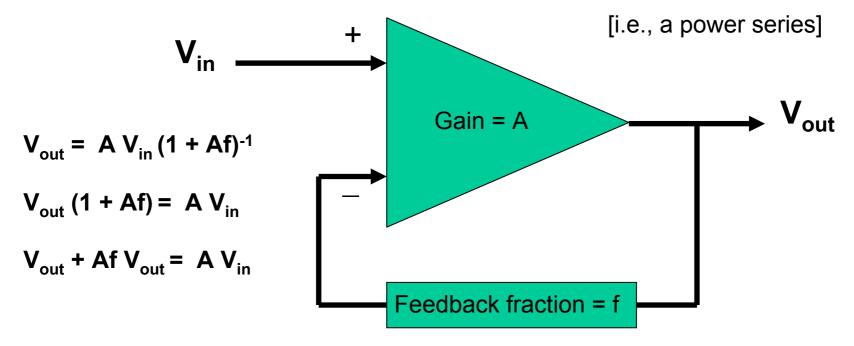
B = Af = Loop gain

G = Overall (closed loop) gain

= Transfer function

$$V_{out} = A V_{in} - (Af) A V_{in} + (Af)^2 A V_{in} - (Af)^3 A V_{in} + (Af)^4 A V_{in} ...$$

$$V_{out} = A V_{in} (1 - Af + (Af)^2 - (Af)^3 + (Af)^4 - ...)$$



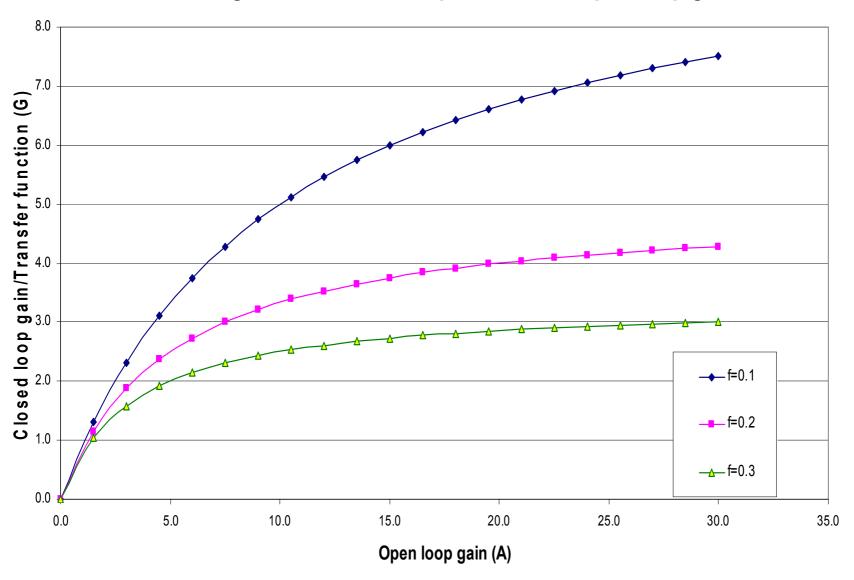
$$V_{out} = A (V_{in} - f V_{out})$$

$$\therefore$$
 G \rightarrow 1/f as A \rightarrow ∞

..
$$G = V_{out}/V_{in} = A / (1+Af) = A/(1+B)$$

so $G << A$, and is "stable" (independent of A)

Negative Feedback: dependence on open loop gain



Positive Feedback

A = Open loop gain f = feedback fraction

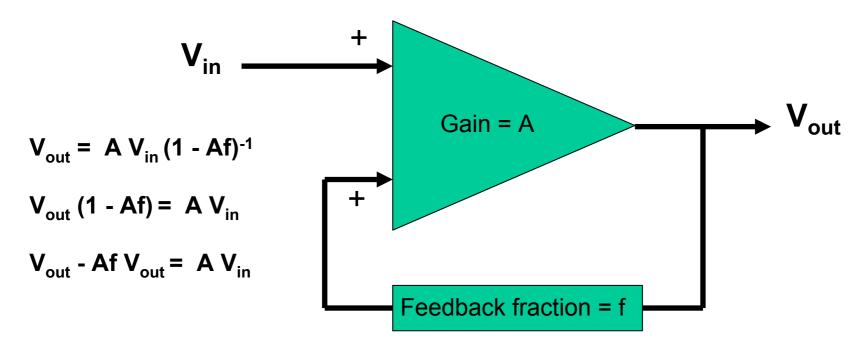
B = Af = Loop gain

G = Overall (closed loop) gain

= Transfer function

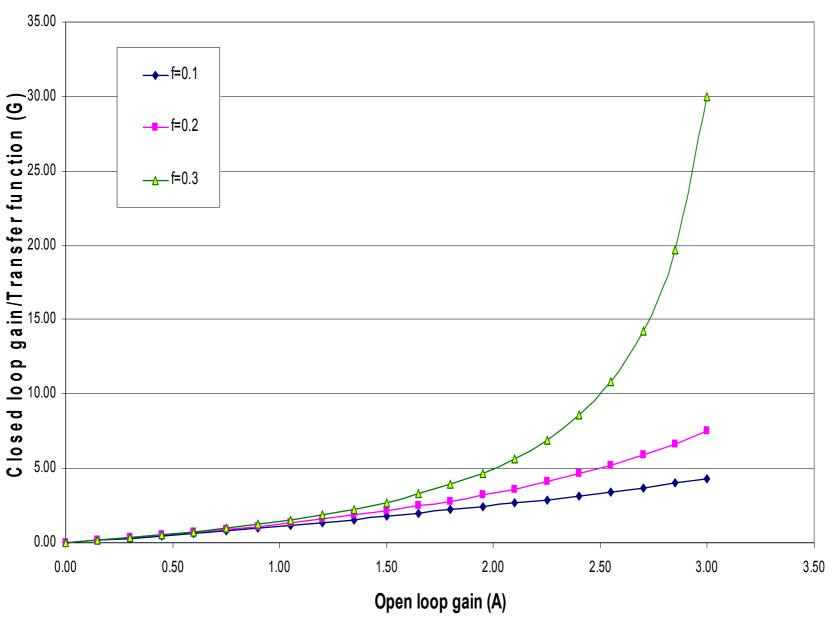
$$V_{out} = A V_{in} + (Af) A V_{in} + (Af)^2 A V_{in} + (Af)^3 A V_{in} + (Af)^4 A V_{in} ...$$

$$V_{out} = A V_{in} (1 + Af + (Af)^2 + (Af)^3 + (Af)^4 + ...)$$



 $V_{out} = A (V_{in} + f V_{out})$ $\therefore G = V_{out}/V_{in} = A / (1-Af) = A/(1-B)$ so G > A, and G $\rightarrow \infty$ as Af \rightarrow 1 i.e. system becomes *unstable*

Positive Feedback: dependence on open loop gain



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